

Application Note 226 Step-Up DC-DC Converter Calibration and Adjustment Using a Digital Potentiometer

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Introduction

The purpose of this application note is to show an example of how a digital potentiometer can be used in the feedback loop of a step-up DC-DC converter to provide calibration and/or adjustment of the output voltage. The example circuit uses a MAX5025 step-up DC-DC converter (capable of generating up to 36V, 120mW max) in conjunction with a DS1845, 256 position, *NV* digital potentiometer. For this example, the desired output voltage is 32V, which is generated from an input supply of 5V. The output voltage can be adjusted in 35mV increments (near 32V) and span a range wide enough to account for resistance, potentiometer and DC-DC converter tolerances (27.6V to 36.7V).

While the intent of this application note is to show an example of a step-up DC-DC converter, the ideas presented here can be applied to generate other combinations of output voltages, step sizes, ranges, and power requirements to meet your particular applications' needs. An additional application note is available (AN225) that shows an example of using a digital potentiometer with a step-down DC-DC converter. A link to AN225 appears at the end of this document.

Fixed Step-up DC-DC Converter

The typical circuit from the MAX5025 data sheet is shown in Figure 1. In this circuit, the output voltage, V_{OUT} , is determined by the ratio of fixed resistors R1 and R2. These two resistors form a voltage divider that feeds a fraction of the output voltage back to the FB pin, creating a closed-loop system. The system is at equilibrium when V_{OUT} is generating the desired output voltage and the R1 and R2 voltage divider feeds back 1.25V to the FB pin. When V_{OUT} is lower than the desired output voltage (and hence the voltage fed back to FB is below 1.25V), the DC-DC converter IC attempts to deliver additional power until FB reaches 1.25V. Equation 1 is directly from the MAX5025 data sheet. Solving Equation 1 for V_{OUT} yields Equation 2 where V_{REF} , the FB Set Point, is 1.25V for the MAX5025.

$$R1 = R2 \left(\frac{V_{OUT}}{V_{REF}} - 1\right)$$
Equation 1
$$V_{OUT} = V_{REF} \left(\frac{R1}{R2} + 1\right)$$
Equation 2

Figure 1. Fixed Step-Up DC-DC Converter Circuit



Digital Potentiometer Considerations

One possible way of adding a digital potentiometer into the feedback loop is shown in Figure 2. However, before selecting a digital potentiometer, a number of considerations must be given some thought. The following list of questions address important design considerations and assist in the device selection process.

- Is a 3V or 5V supply available for the potentiometer? The majority of digital potentiometers available require 3V or 5V to operate. Likewise, the voltage needs to be available before V_{OUT} can be generated. Since the example circuit has a 5V input supply, this is not a concern here but if V_{IN} were larger, this would be a major concern.
- 2. Will the system only be calibrated once? Or monitored/controlled closed loop? How will the digital potentiometer be controlled? Using a microcontroller? Push-button? *The answer to these questions will help select a specific digital potentiometer. For example, if the system is going to be calibrated once, say during production testing, then a NV (NV) potentiometer is needed to save the calibrated wiper position. Likewise, it is also important to consider how the potentiometer will be programmed. Will it be programmed with a production tester capable of talking 2-wire or 3-wire, or is a push-button potentiometer needed?*
- 3. How many steps are needed? What resolution is required? What range is needed? These answers determine the minimum acceptable number of potentiometer positions and serve as a benchmark when experimenting with different resistor values when finding a combination that is acceptable even in worst case conditions due to resistor/component tolerances. Furthermore, be aware that the desired output voltage range will be different than the actual output range so that the desired range can also be obtained even when using worst-case tolerances.
- 4. What is the max voltage that will ever be applied to the potentiometer terminals? Is V_{REF} (V_{FB}) larger than the maximum allowable voltage on the V_W pin? Some potentiometers have a specification that states the maximum allowable voltage than can be applied to any of the potentiometer terminals. The second question is intended to be a sanity check. For example, the MAX5027 (not the MAX5025) has a V_{REF} of 30V! This voltage cannot be applied to the wiper terminal. The reason V_{REF} is so high is because it is a non-adjustable DC-DC converter.

- 5. Is the FB pin bias current large enough to cause a noticeable drop across the wiper resistance, R_W? Does the FB pin bias current exceed the maximum (or abs max) wiper current specification? *Fortunately, the maximum wiper current specification is usually 1mA or larger, while the bias current is in the magnitude of nA. The second reason why the bias current is important is because if too large, the voltage drop across the wiper resistance becomes noticeable and should be accounted for when calculating the output voltage.*
- 6. Does the minimum and maximum position of the potentiometer connect directly to V_L and V_H? For example, the DS1805 is different in that the maximum potentiometer setting (255) does not connect directly to the H terminal. It is actually one resistor (LSB) away from the H terminal. Granted, the difference between 255 and 256 resistors are nil, the same is not the case for potentiometers with fewer positions. The result of this question can be seen later in Equation 4.
- What is the desired tolerance of V_{OUT}? 5%? 10%? 3%? Keep in mind that the DC-DC converter IC itself has a tolerance. The MAX5025 for example has a tolerance of 5%. And this is completely independent from the tolerance of R1 and R2, which may also be 5% or 1%. These tolerances will be discussed in detail later.
- 8. What is the operating temperature range of the circuit? Just as important as knowing the effects of the tolerances, it is equally important to know the effects of temperature on the output voltage.

Figure 2. Digital Potentiometer in the Voltage Divider Feedback Path



Adding a Digital Potentiometer to the Feedback Path

Although there are several ways that a digital potentiometer could have been added to the circuit in Figure 1, this application note will only discuss the voltage divider configuration as shown in Figure 2. Two configurations that will not be discussed are 1) using the pot as a variable resistor (by connecting the wiper terminal to either the high or low terminal) between R1 and R2, and 2) eliminating R2 and connecting the pot low terminal to ground.

Equations 3, 4, and 5 show the relation of the potentiometers' position to R_L , R_H , and R_{POT} . Once a potentiometer is added into the feedback loop, these equations can be used to modify Equations 1 and 2 to represent the new circuit.

$$R_{POT} = R_{H} + R_{L}$$
Equation 3

$$R_{L} = current \ potentiometer \ position \times \left(\frac{R_{POT}}{(total \ number \ of \ pot \ positions - 1)}\right)$$
Equation 4

$$R_{H} = R_{POT} - R_{L}$$
Equation 5

 R_{POT} is the end-to-end resistance of the potentiometer and R_H and R_L are dependent on the current wiper position setting (see Figure 2). The denominator of Equation 4 is *(total number of pot positions -1)* if the max and min wiper positions connect directly to the H and L potentiometer terminals, which is true for the DS1845. Some digital potentiometers may have an additional resistor between the max potentiometer setting and the H terminal. The denominator for those potentiometers would not include the -1 and simply be *(total number of pot positions)*.

Equation 2 becomes,

$$V_{OUT} = V_{REF} \left(\frac{R1 + R_{H}}{R2 + R_{L}} + 1 \right)$$
 Equation 6

Resistor Calculations

Unfortunately, there is no quick, easy way of calculating R1 and R2. V_{OUT} is a function of multiple variables and many solutions exist. Choosing the optimal solution for a particular application involves a decent amount of trial and error. For this reason, a spreadsheet is the single most valuable tool because it allows the designer to make a tweak and instantly see its effects on V_{OUT} for a single potentiometer position as well as a sweep of the entire potentiometer range. The following will describe the process used to calculate the values for the example circuit generating 32V.

Assumptions made up front for this design were, $R_{POT} = 10k\Omega$, 256 positions, $V_{REF} = V_{FB} = 1.25V$, and the output voltage will be 32V when the pot is set in the middle position (position 127). The spreadsheet created for this application note can be found on the Dallas Semiconductor ftp site. A link to the spreadsheet can be found at the end of this application note. Plugging the assumptions into Equations 4 and 5, and then into Equation 6 determines the needed ratio between R1 and R2.

$$\frac{V_{OUT}}{V_{REF}} - 1 = \left(\frac{R1 + 5019.6}{R2 + 4980.4}\right) = \frac{32}{1.25} - 1 = 24.6$$
 Equation 7

The MAX5025 data sheet says to choose an R2 in the $5k\Omega$ to $50k\Omega$ range and then calculate R1. However, how can one make an educated R2 selection in such a large range without knowing what else will be effected? The spreadsheet shown in Figure 3 was created specifically for this. Simply type in a value for R2 in the red cell (D7). R1 is then automatically calculated to obtain the ratio in cell Q7 (which was the result of Equation 7). In addition, thousands of other calculations are also performed and then V_{OUT} vs. Pot Position is plotted. The V_{OUT} vs. Pot Position plot shows the expected output voltage for all 256 potentiometer positions. Linearity, range, and slope can all be seen clearly. Look for the trace labeled "Typical". The other traces will be described later. Comparing plots of R2 = $5k\Omega$ and R2 = $50k\Omega$ (Figure 4) it can be seen that smaller values of R2 (Figure 4a) produce a much larger output range, although non-linear and having a steep slope. The steep slope produces larger than desired step sizes (especially at the lower potentiometer positions)

decreasing the resolution of V_{OUT} . Larger values of R2, on the other hand, produce a linear output and much smaller slope (Figure 4b). The smaller the slope, the smaller the step size (and hence resolution). When attempting to "fine-tune" a particular output voltage, it is desirable to have many potentiometer positions at and around the desired output voltage. The drawback, which will be discussed in the following section, is that since R1 and R2 have a tolerance of ±1%, there is a possibility that no potentiometer setting will reach 32V. This can be seen looking at the top trace in Figure 4b. When the potentiometer is set to position 0, the output voltage is ~37.5V and when the potentiometer is set to position 255, the output only goes down to 32.3V. Therefore, it is important to find a happy medium. For the example circuit, the happy medium (determined by trial and error, entering various values of R2 and looking at the V_{OUT} vs. Pot Position graph ensuring that 32V could be reached in all conditions with an acceptable step size) is 30k Ω . The closest 1% SMT standard value is 30.1k Ω . Plugging this value into the spreadsheet and having it recalculate R1, the closest standard value had to be found for R1 as well. The graph shown in Figure 3 shows that 32V can be obtained even in the worst-case conditions.

	A	В	С	D	E	F	G	Н	1	J	к	L	M	N	0	Р	Q	R	S
1																			
2	Set Ext R2		D4 100														B W A	0011	
3			R1 and R2 are standard		11% values.												Position fo		
4			1							Em D1		Ent D2 Ente	- (11-0)	Detfeeds	a an d) Dania		127	4980.392	
6	potpos	pot value	1% Ext R1 Ext R2			Vref (min)	Vect (tup)	Vref (max)			1 Error (1%) Ext R Max Min		Error (1%) Pot (end t Max Min		o end) Resistance Max		B1/B2 ratio so 7Fh = 3		24
7	256	10000				1.19	1.25	1.31		Min 836550				8000 12000		24.6		/ so / Fri = 3.	
8	206	10000	738000	30000	ratio lo	ratio lo				036000				0000	12000	Value		ide of each	
9	notnoc	RL			pot min	pot max	ratio high pot min	ratio high	tup		Delta between r lo, p min	rlo, pimax		r ki namov			oltage on high side of pot in _r lo, p max_r hi, p mir		chip may
10	pot pos 0	0	36,75664	pot% 0	34.2486	34.40517	39,18038	pot max 39.35623	typ		rio, prim	rio, pinax	Trin, p trint	Thi, pittax	1.665282			1.66169	1.837534481
11	1	39.21569	36,70882	0.003922	34,21329	34.352	39,13918	39,29417	-0.047826		-0.035306675	-0.053175	-0.041206	-0.062054	1.663116		1.657156	1.659942	1.834637207
12	2		36.66112	0.007843	34,17806	34.29899	39.09806	39,23231	-0.047702		-0.035233955				1.660954	1.500052		1.658198	1.831749055
13	3	117.6471	36.61354	0.011765	34,1429	34.24614	39.05702	39,17065	-0.047578		-0.03516146		-0.041033		1.658799	1.498508	1.65205	1.656458	1.828869982
14	4	156.8627	36,56608	0.015686	34,10781	34,19346	39.01608	39,10918	-0.047455		-0.035089188	-0.052685	-0.040947	-0.06147	1.656649	1.496968	1.649508	1.654721	1.825999945
15	5	196.0784	36.51875	0.019608	34.07279	34,14093	38.97521	39.0479	-0.047332		-0.035017138				1.654505		1.646974	1.652988	1.823138902
16	6	235.2941	36.47154	0.023529	34.03785	34.08857	38.93444	38,98682	-0.047209	1									1.82028681
17	7	274.5098	36.42446	0.027451	34.00297	34.03637	38.89375	38,92592	-0.047087					DOT	POSITION				1.817443629
18	8	313.7255	36.37749	0.031373	33,96817	33.98433	38.85314	38.86522	-0.046966				T +#1	vs. PUT	FUSITION	4			1.814609315
19	9	352.9412	36.33065	0.035294	33,93344	33.93245	38.81262	38.8047	-0.046845										1.811783827
20	10	392,1569	36.28392	0.039216	33.89878	33.88072	38.77219	38,74437	-0.046725		Chart Area	.							1.808967125
21	11		36.23732	0.043137	33,86419	33.82915	38,73183	38.68423	-0.046604			1				 Typical 			1.806159167
22	12	470.5882	36,19083	0.047059	33,82967	33.77774	38.69157	38.62428	-0.046485		40 +++						1in/ Pot Mit	1	1.803359913
23	13	509.8039	36.14447	0.05098	33,79522	33.72649	38.65138	38,56451	-0.046366		39 🦄								1.800569322
24	14	549.0196	36.09822	0.054902	33,76084	33.67539	38.61128	38,50492	-0.046247								lin/Pot Ma		1.797787355
25	15	588.2353	36.05209	0.058824	33,72653	33.62445	38.57126	38.44552	-0.046129		38 +++		++++	++++			1ax/Pot Mit	1	1.795013971
26	16	627.451 666.6667	36.00608 35.96018	0.062745	33.6923 33.65813	33.57366 33.52302	38.53133 38.49147	38.38631 38.32727	-0.046011 -0.045894		37					× Ratio N	1ax/Pot Ma		1.79224913 1.789492794
27	17	705.8824	35.96018	0.056567	33,65813	33.52302	38.49147	38.32727 38.26842	-0.045894		- " N					B1-84	5k (1%),	1	1.789492794
20	19	705.8824	35,86875	0.070588	33,58999	33.47203	38,41201	38.20974	-0.045777		36 🕂		4 				uk (1%).	-	1.784005477
30	20	784.3137	35.8232	0.078431	33,55603	33.37202	38,37241	38,15125	-0.045545		35						10k (20%),		1.78127442
31	21	823,5294	35.77777	0.082353	33,52214	33.32199	38.33288	38.09294	-0.045429			Турі	cal			Vre = 1.3	25V (5%)	1	1.778551711
32	22	862.7451	35.73246	0.086275	33,48831	33.27211	38.29344	38.0348	-0.045314		a 34 🕂	+++						-	1.775837313
33	23	901.9608	35.68726	0.090196	33,45456	33.22237	38,25408	37.97684	-0.045199		ີເຼີ								1.773131187
34	24	941.1765	35.64217	0.094118	33,42087	33.17279	38.2148	37,91906	-0.045085		5 ³³							1	1.770433297
35	25	980.3922	35,5972	0.098039	33.38724	33,12335	38,17559	37.86145	-0.044972		> 32 🕂	+++						-	1.767743604
36	26	1019.608	35.55234	0.101961	33,35369	33.07406	38,13647	37.80402	-0.044858										1.765062071
37	27	1058.824	35,5076	0.105882	33.3202	33.02492	38.09743	37.74676	-0.044745		31		t t					1	1.762388661
- 38	28	1098.039	35.46297	0.109804	33,28678	32.97592	38.05847	37.68967	-0.044633		30	++++	+++				++++		1.759723337
39	29	1137.255	35.41845	0.113725	33.25343	32.92707	38.01959	37.63276	-0.044521										1.757066063
40	30	1176.471	35.37404	0.117647	33.22015	32.87837	37.98079	37.57602	-0.044409		29			┽╋╎╉				1	1.754416802
41	31	1215.686	35.32974	0.121569	33,18693	32.8298	37.94207	37.51944	-0.044298		28								1.751775518
42	32	1254.902	35.28555	0.12549	33,15377	32,78138	37,90342	37.46304	-0.044187									•	1.749142175
43	33	1294.118	35.24147	0.129412	33,12069	32,7331	37.86486	37.40681	-0.044077		27				+++				1.746516737
44	34	1333.333	35,19751	0.133333	33.08767	32,68497	37.82637	37.35075	-0.043967										1.743899169
45 46	35	1372.549 1411.765	35.15365 35.1099	0.137255 0.141176	33.05471 33.02182	32.63697 32.58912	37.78796	37.29485 37.23913	-0.043857 -0.043748		26							1	1.741289435
46	36	1411.765	35,1099	0.141176	33.02182	32.58912 32.54141	37.74963	37.23913	-0.043748		25								1.7386875
47	37	1450.98	35.06626	0.145098	32,989	32.59191	37.6732	37,18356	-0.043539		0	50		100	150	200	250)	1.73505333
49	39	1529.412	34.97931	0.14302	32,90624	32.43363	37.63511	37.07294	-0.043531		5					200	20.	-	1.730928144
50	40	1568.627	34,93599	0.156863	32.89092	32.3991	37,59708	37.01234	-0.043315				PC	OT POSITI	ON (DEC)				1.728357059
51	41	1607.843	34,89279		32 85835	32 35 194	37 55914	36 96297							1 15808 (9	144/141	L SEUEZ C	1592931	1 725793601

Figure 3. Example Resistor and Error Spreadsheet Screenshot

Once values for R1 and R2 are selected, it is important to verify that V_H does not exceed the maximum specification (of $V_{CC} + 0.5V$ for the DS1845). V_H can be calculated using Equation 8.

$$V_{\rm H} = \frac{V_{\rm OUT}}{\left(R1 + R2 + R_{\rm POT}\right)} \times \left(R2 + R_{\rm POT}\right)$$
Equation 8

Figure 5 shows a screenshot of the bottom of the example spreadsheet. The calculation of V_H can be seen on the far right along with the max voltage across the potentiometer. We can see that for the resistor values we chose V_H has a worst case potential of 1.84V. This voltage is well within the recommended operating conditions. Other items in interest in Figure 5 are V_{OUT} min/max, min/max deltas between pot positions, and also min/max V_H . While some of the data and calculations shown in the spreadsheet may appear to be of little use, it provides multiple sanity checks to ensure a good design.

Figure 4. R2 Comparison



Figure 5. Additional Calculations

262	252	9882.353	27.67158	0.988235	27.18028	24.7505	30.96512	28,1526	-0.027168		-0.022278334	-0.027592	-0.025786	-0.031839	1.253678	1.192924	1.193975	1.31327	1.31443953			
263	253	9921.569	27.64447	0.992157	27.15804	24.72297	30.93938	28,12084	-0.027114		-0.022241873	-0.02753	-0.025743	-0.031767	1.25245	1.191948	1.192647	1.312178	1.312956347			
264	254	9960.784	27.61741	0.996078	27.13583	24.6955	30.91368	28.08914	-0.027061		-0.022205501	-0.027469	-0.025701	-0.031695	1.251224	1.190973	1.191322	1.311088	1.311476508			
265	255	10000	27.5904	1	27.11366	24.66809	30.88802	28.05752	-0.027008		-0.022169218	-0.027408	-0.025658	-0.031624	1.25	1.19	1.19	1.31	1.31			
266																						
267			Vout	min	27.11366	24.66809	30.88802	28.05752	-0.047826	delta bet	-0.02765228	-0.037243	-0.032123	-0.043177	1.665282	1.503148	1.659721	1.66169	1.837534481	<- max Vh		
268				max	34.2486	34.40517	39,18038	39.35623	-0.027008	%(32V)	-0.086413374	-0.116386	-0.100385	-0.13493	0.415282	0.313148	0.469721	0.35169	0.527534481	<- max voltage across p		pot
269																			6.59418E-05	<- max end-	to-end curr	ent

Error Analysis

Up to this point, all calculations have used typical (nominal) values. However, to ensure the design is production worthy it is essential to calculate the variations of the output voltage due to component tolerances, temperature variations, and any other sources of error and ensure that the desired output voltage can always be obtained. This application note will go as far as analyzing the effects of resistor, potentiometer, and V_{REF} tolerances. The analysis of temperature variations, however, is saved for a future application note.

The MAX5025 V_{REF} has a tolerance of ±5%. This means that the 1.25V could actually be anywhere between 1.19V and 1.31V. What makes this tolerance different than that of the resistors and potentiometer is that this 5% is for the entire temperature range. The resistors and potentiometer on the other hand spec both a tolerance and a temperature coefficient. Resistors R1 and R2 both have a tolerance of ±1%. The tolerance of the DS1845 is ±20%.

Referring back to Figure 3, the use of these tolerances can be seen in row 7 of the spreadsheet. For example, C7 is the nominal value of R1, while J7 is nominal (C7) minus 1% and K7 is the nominal plus 1%. Once this is done for all of the tolerances, calculations can easily be repeated multiple times, calculating all possible combinations in search of the combinations that yield the minimum and maximum output voltages. These combinations can then be added to the V_{OUT} vs. Pot Position plot and verified that each can generate 32V. Once all of the traces on V_{OUT} vs. Pot Position graph meets the desired specifications, the resistor selection is complete. Figure 6 shows the final circuit with the DS1845 and with the selected values of R1 and R2. The V_{OUT} vs. Pot Position plot for this circuit is shown in Figure 3.



Figure 6. Final Circuit Using a DS1845 Digital Potentiometer

Conclusion

This application note shows an example of how to use a digital potentiometer in the feedback loop of a stepup DC-DC converter to allow the output voltage to be calibrated. While this application note specifically uses the MAX5025 and the DS1845 to generate 32V, the concepts presented here can be applied towards other potentiometer/converter combinations as well as other output voltages and power ratings.

Questions/comments/suggestions concerning this application note can be sent to: MixedSignal.Apps@dalsemi.com.

Link to the spreadsheet used in this example: <u>ftp.dalsemi.com/pub/system_extension/pots/AN226/AN226.xls</u>

Link to Application Note 225 showing a step-down DC-DC converter: <u>http://pdfserv.maxim-ic.com/arpdf/AppNotes/app225.pdf</u>

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